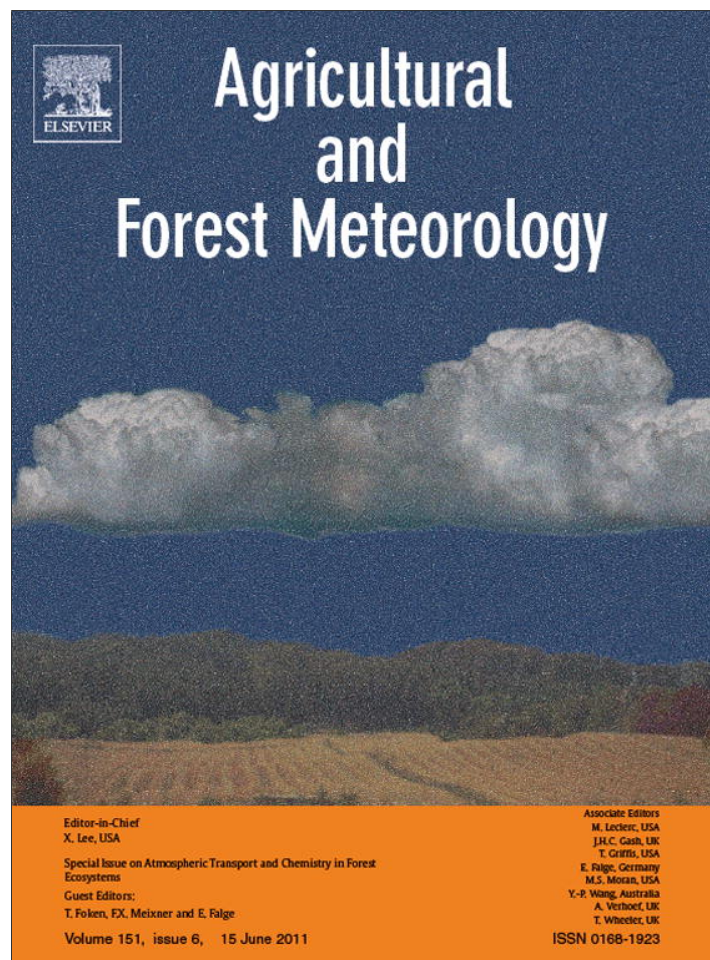


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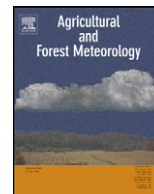
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# Measured deuterium in water vapour concentration does not improve the constraint on the partitioning of evapotranspiration in a tall forest canopy, as estimated using a soil vegetation atmosphere transfer model

Vanessa Haverd<sup>a,b,\*</sup>, Matthias Cuntz<sup>c,d,e</sup>, David Griffith<sup>b</sup>, Claudia Keitel<sup>c,f</sup>, Carol Tadros<sup>g</sup>, John Twining<sup>g</sup>

<sup>a</sup> CSIRO Marine and Atmospheric Research, GPO Box 3023, Canberra, ACT 2601, Australia

<sup>b</sup> Department of Chemistry, University of Wollongong, NSW 2522, Australia

<sup>c</sup> Environmental Biology Group, Research School of Biology, GPO Box 475, Canberra, ACT 2601, Australia

<sup>d</sup> Max-Planck-Institut für Biogeochemie, Hans-Knöll-Str. 10, 07745 Jena, Germany

<sup>e</sup> UFZ – Helmholtz Centre for Environmental Research, Permoserstr. 15, 04318 Leipzig, Germany

<sup>f</sup> Faculty of Agriculture, Food & Natural Resources, University of Sydney, Eveleigh, NSW 2015, Australia

<sup>g</sup> Institute for Environmental Research, Australian Nuclear Science and Technology Organisation (ANSTO), Menai, NSW 2234, Australia

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## ABSTRACT

Partitioning the evapotranspiration (*ET*) flux in a forest into its component fluxes is important for understanding the water and carbon budgets of the ecosystem. We use non-linear parameter estimation to determine the vertical profile of the Lagrangian timescale ( $T_L$ ) and partitioning of *ET* that simultaneously optimise agreement between modelled and measured vertical profiles of temperature, water vapour, carbon dioxide concentrations, and deuterated water vapour for a two-week period in November 2006. High precision real-time trace gas measurements were obtained by FTIR spectroscopy. Modelled temperature and concentration profiles are generated using a Lagrangian dispersion theory combined with source/sink distributions of HDO, H<sub>2</sub>O, sensible heat, and CO<sub>2</sub>. These distributions are derived from an isotopically enabled multilayer Soil Vegetation Atmospheric Transfer (SVAT) model subject to multiple constraints. The soil component of the model was tested in isolation using measured deuterium content of soil chamber evaporate, while the leaf component was tested using isotopic analyses of leaf and xylem water, combined with leaf-level gas exchange measurements. Optimisation of  $T_L$  and the partition of *ET* was performed twice: once using only temperature, H<sub>2</sub>O and CO<sub>2</sub> profiles and a second time including HDO as well. The modelled vertical concentration profiles resulting from inclusion of HDO in the cost function demonstrate our ability to make consistent estimates of both the scalar source distributions and the deuterium content of the water vapour sources. However, introducing measurements of deuterium in water vapour does not significantly alter resulting estimates of normalised  $T_L$  ( $0.4 \pm 0.1$  at canopy top) and the partition of *ET* ( $85 \pm 2\%$  transpiration), suggesting that the additional data and modelling required to use deuterium are not warranted for the purpose of partitioning *ET* using the framework presented here.

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## 1. Introduction

Understanding the strong coupling between water and carbon fluxes in ecosystems requires a detailed understanding of the individual component fluxes. For water, transpiration (*T*) and evaporation (*E*) can be separated with different combinations of lysimeters, porometers, Bowen ratio, eddy-covariance, and sap flow measurements. All these methods bear large uncertainties

(e.g. Herbst et al., 1996). Using observations of the stable isotopic composition of water vapour exchanged between vegetation and the atmosphere in conjunction with the classical methods above can potentially reduce associated errors (e.g. Williams et al., 2004). This is because the isotopic composition of the water in the individual components can be quite distinct and the fluxes are therefore isotopically tagged. However, most isotope-based separations of transpiration and evaporation do assume isotopic steady-states in soil and vegetation (Ferretti et al., 2003; Moreira et al., 1997; Williams et al., 2004; Xu et al., 2008; Yakir and Wang, 1996; Yezpe et al., 2005). This assumption neglects significant isotopic gradients from stomata to xylem and within the soil column (e.g. Allison and Barnes, 1983; Farquhar et al., 1993; Yakir and Sternberg, 2000),

\* Corresponding author at: CSIRO Marine and Atmospheric Research, GPO Box 3023, Canberra, ACT 2601, Australia. Tel.: +61 2 6246 5981; fax: +61 2 6246 5988.  
E-mail address: [Vanessa.Haverd@csiro.au](mailto:Vanessa.Haverd@csiro.au) (V. Haverd).

potentially leading to biases in the isotope-derived component fluxes.

In the previous work (Haverd et al., 2009) (hereafter Hav09), we simultaneously estimated the partitioning of evapotranspiration ( $ET$ ) between ground and canopy, together with the turbulent Lagrangian timescale ( $T_L$ ) in a 40 m tall Eucalyptus forest in south-eastern Australia for a two-week campaign period. This was done by optimising modelled vertical scalar concentration profiles (potential temperature ( $\theta$ ), water vapour and  $CO_2$ ) against corresponding measurements. Inputs to the predicted profiles were source/sink distributions from a Soil Vegetation Atmosphere Transfer (SVAT) model, and vertical profiles of the turbulence statistics, namely the standard deviation of the vertical wind velocity ( $\sigma_w$ ) and  $T_L$ . Of these, the largest uncertainties were in the ground/canopy partitions of sensible and latent heat fluxes, and hence the evapotranspiration partition between ground and canopy, and in  $T_L$ . SVAT model predictions of net fluxes of  $CO_2$ , water vapour and sensible heat were well constrained by measured fluxes above the canopy, the ground/canopy partition of  $CO_2$  was well-constrained by 2 independent sets of ground chamber measurements, and  $\sigma_w$  was measured. Therefore two parameters specifying the vertical profile of  $T_L$  and one parameter for modifying the SVAT model predictions of the ground/canopy sensible and latent heat flux partitions were optimised. This led to agreement between observed and predicted concentrations to within the 95% confidence limits for most of the hourly mean profiles, and to revised estimates of  $T_L$  and ground/canopy partitions of sensible and latent heat fluxes.

In the current work, we build on the analysis in Hav09 by including vertical profiles of deuterium isotopic content ( $\delta D$ ) in water vapour in addition to those of potential temperature, water vapour and  $CO_2$  concentrations, which were used previously.  $\delta D$  is defined as:

$$\delta D = \frac{[HDO]_{\text{sample}}/[H_2O]_{\text{sample}}}{[HDO]_{\text{ref}}/[H_2O]_{\text{ref}}} - 1 \quad (1)$$

where the reference material is V-SMOW (Gonfiantini, 1978). The objective is to use  $\delta D$  to provide an additional constraint on the estimates of  $T_L$  and ground/canopy partitions of sensible and latent heat fluxes. This extension requires measured vertical profiles of  $\delta D$  in atmospheric water vapour and an isotopically enabled SVAT model, capable of predicting  $\delta D$  in the soil evaporate and transpire.

In Section 2, we describe our approach for simultaneously constraining estimates of  $T_L$  and the partition of evapotranspiration. Section 3 describes the field measurements. In Section 4 we describe the isotopically enabled SVAT model, including its validation against measurements of  $\delta D$  in leaf water and soil evaporate within a chamber. We also present predictions from the validated model of the  $CO_2$ , sensible heat and latent heat sources and  $\delta D$  in  $ET$  for the ground and canopy. In Section 5, we compare predicted and observed vertical concentration profiles and evaluate the additional constraint provided by  $\delta D$  profiles on our final estimates of  $T_L$  and the ground/canopy partition of  $ET$ .

## 2. Approach to using vertical concentration profiles to constrain the ground/canopy partition of $ET$ and the turbulent Lagrangian time scale

The relationship between the vertical distribution of scalar source/sinks and scalar concentrations within plant canopies may be written:

$$c_i - c_{\text{ref}} = \sum_{j=1}^m D_{ij} S_j \Delta z_j \quad (2)$$

in which  $c_i$  and  $c_{\text{ref}}$  are the concentration at height above the ground  $z_i$ , and at a reference height ( $z_{\text{ref}}$ , typically above the canopy),  $S_j$  is the source/sink strength at height  $j$  distributed across a layer of thickness  $\Delta z_j$ , and  $D_{ij}$  are the elements of the dispersion matrix relating  $c_i$  to  $S_j$ .

Eq. (2) requires  $D$  and  $S$ . In order to use it to estimate parameters specifying the partition of  $ET$  and  $T_L$ , we require: (i)  $D$  as a function of  $T_L$ , and a parametric form of the vertical profile of  $T_L$  within the canopy; (ii) specification of  $S$ , and a parameter which can be used to correct the prior estimate of the ground/canopy partitions of sensible and latent heat fluxes and hence of  $ET$ ; (iii) specification of the parameter estimation procedure, including the search strategy and formulation of the cost function to be minimised. Below we discuss how these requirements are met.

### 2.1. In-canopy dispersion

Calculation of the dispersion matrix  $D$  requires knowledge of  $\sigma_w$ , the vertical profile of the standard deviation of vertical velocity, and  $T_L$ , the Lagrangian time scale. We adopt the widely used Localised Near-Field (LNF) theory of Raupach (1989a,b), and restrict our analysis to times when this theory applies (i.e. periods of fully coupled flow: see Section 3.1). The concentration in Eq. (2) is expressed as the sum of near-field and far-field components ( $c_i = c_{ni} + c_{fi}$ ). The diffusive far-field component,  $c_{fi}$ , provides large-scale variation in the concentration profile, upon which is superimposed detailed local structure due to  $c_{ni}$ , the non-diffusive near-field component. The dependences of the near- and far-field concentration components (and hence  $D$ ) on  $\sigma_w$  and  $T_L$  are as follows.

The continuous forms of the near- and far-field concentration components depend on  $\sigma_w$  and  $T_L$  as:

$$c_n(z) = \int_0^\infty \frac{S(z_s)}{\sigma_w(z_s)} \left\{ k_n \left[ \frac{z - z_s}{\sigma_w(z_s) T_L(z_s)} \right] + k_n \left[ \frac{z + z_s}{\sigma_w(z_s) T_L(z_s)} \right] \right\} dz_s \quad (3)$$

$$c_f(z) = c_f(z_{\text{ref}}) + \int_z^{z_{\text{ref}}} \frac{F(z')}{K_f(z')} dz' \quad (4)$$

In Eqs. (3) and (4),  $z_s$  is the source height;  $z_{\text{ref}}$  is an arbitrary reference height,  $k_n$  is a 'near-field kernel' approximated by:  $k_n(\zeta) = -0.3989 \ln(1 - e^{-|\zeta|}) - 0.1562 e^{-|\zeta|}$ ;  $c_f(z_{\text{ref}}) = c(z_{\text{ref}}) - c_n(z_{\text{ref}})$ ;  $F(z)$  is the flux density, related to the source strength by  $F(z) = \int_0^z S(z') dz'$  and to the far-field concentration by the gradient diffusion relationship  $F(z) = -K_f(z)(dc_f/dz)$ , where  $K_f$  is the far-field diffusivity,  $K_f(z) = \sigma_w^2(z) T_L(z)$ .

To calculate the elements  $D_{ij}$  we follow Raupach (1989a). Consider a scalar that is released uniformly in layer  $j$  with source strength,  $S_j$ , but with zero strength in all other layers. The resulting partial concentration profile  $c_i$  defines the elements of the dispersion matrix for dispersion from layer  $j$  to concentration at height  $z_i$ , i.e.

$$D_{ij} = \frac{c_i - c_R}{S_j \Delta z_j} \quad (5)$$

Each element of  $D_{ij}$  has a near field and a far field component because  $c_i = c_{ni} + c_{fi}$ .

We assume a unit source strength in each layer and use Eqs. (3) and (4) to estimate  $c_{ni}$  and  $c_{fi}$  and hence the coefficients  $D_{ij}$  from Eq. (5), provided we know  $\sigma_w(z)$  and  $T_L(z)$ .

While  $\sigma_w(z)$  is measurable, the vertical profile of  $T_L$  is not. Our prior estimate of the  $T_L$  profile is a fit of Eq. (6) (Styles et al., 2002):

$$\frac{T_L(z) u_*}{h_c} = c_2 \frac{1 - \exp(-c_1 z/h_c)}{1 - \exp(-c_1)} \quad (6)$$

to the single-point estimate of the Eulerian time scale ( $T_E$ ):

$$T_L = \frac{\beta \bar{u} T_E}{\sigma_w} \quad (7)$$

with

$$T_E = \int_0^\infty \frac{w'(t)w'(t + \tau)}{\sigma_w^2} d\tau \quad (8)$$

where  $w' = w - \bar{w}$  is the instantaneous deviation of the vertical wind velocity,  $w$ , from its time-averaged value,  $\bar{w}$ .  $\bar{u}$  is the mean horizontal wind speed and  $\beta$  is a constant of order 1 (Raupach, 1989a). As in Hav09, we set  $\beta$  to 1 and obtained the velocity statistics from a vertical array of 3D sonic anemometers.

## 2.2. Source/sink distributions

We use an isotopically enabled SVAT model to estimate the vertical source/sink distributions of CO<sub>2</sub>, sensible heat, water vapour (H<sub>2</sub>O) and deuterated water vapour (HDO). The predicted net fluxes of CO<sub>2</sub>, sensible heat and H<sub>2</sub>O are constrained by measurements of these quantities above the canopy, and the ground source of CO<sub>2</sub> is constrained by chamber measurements. Unlike CO<sub>2</sub>, the ground sources of water vapour and sensible heat are not measured. Therefore we treat the SVAT modelled ground/canopy partitions of these quantities as prior estimates and introduce a partition correction parameter,  $x_{\lambda E}$ . The corrected latent heat flux ( $\lambda E$ ) at the soil is set to  $(1 + x_{\lambda E})\lambda E_{soil}^0$  where  $\lambda E_{soil}^0$  is the SVAT model output value, and the prior estimate of  $x_{\lambda E}$  is zero. In order to conserve the total heat flux at the soil surface, the sensible heat flux at the ground ( $H_{soil}$ ) was set to  $H_{soil}^0 - x_{\lambda E}\lambda E_{soil}^0$ . Also, canopy contributions to the latent and sensible heat fluxes were modified to conserve net  $H$  and  $\lambda E$  (cf. Hav09). The same partition correction parameter was applied to prior estimates of the ground and canopy sources of HDO.

## 2.3. Parameter estimation

The Gauss–Levenberg–Marquardt method is used in the optimisation process, as implemented in the model-independent parameter estimation software, PEST (Doherty, 1999). The cost function to be minimised in this process is the sum of partial costs  $\Phi_\nu$  where  $\nu$  refers to the atmospheric variable being fitted ( $\theta$ , H<sub>2</sub>O, CO<sub>2</sub>,  $\delta D$ ). The  $k$ th observation for each fitted variable is constructed as the average of  $n_{\nu,k}$  ensemble members (see Section 3). Each partial cost function is defined in terms of a weighting,  $w_{\nu,k}$ , for each observation and a residual between the observation and prediction,  $r_{\nu,k}$ :

$$\Phi_C = \sum_{k=1}^{n_{obs,\nu}} (w_{\nu,k} r_{\nu,k})^2 \quad (9)$$

where  $n_{obs,\nu}$  is the number of observations for each variable. We specify the weightings, such that each concentration type contributes equally to the prior cost, and each observation is weighted by the number of ensemble members,  $n_{\nu,k}$ , contributing to it. This leads to:

$$w_{\nu,k} = \sqrt{\frac{n_{\nu,k}/N_\nu}{\sum_{i=1}^{n_{obs,\nu}} n_{\nu,i} r_{\nu,i}^2}} \quad (10)$$

where  $N_\nu$  is the number of concentration types.

## 3. Measurements

Measurements other than those of the isotopic species are described in Hav09 and summarised briefly below. The analysis of trace gases and their isotopologues by FTIR spectroscopy is novel

and is described in the appendix. We describe the new isotopic measurements in more detail: firstly the measurement of vertical profiles of  $\delta D$  in atmospheric water vapour, followed by the auxiliary measurements used to independently validate the leaf-level and soil components of the isotopically enabled SVAT model.

### 3.1. Tower measurements

Measurements were made in a 40 m tall temperate Eucalyptus forest at the Tumbarumba Ozflux site (35.6557°S, 148.1521°E, elevation 1200 m) in southeast Australia. Hourly vertical flux densities of CO<sub>2</sub> ( $F_c$ ), latent heat ( $\lambda E$ ) and sensible heat ( $H$ ) were measured continuously using the eddy covariance technique, with sensors mounted on top of a 70 m mast (Leuning et al., 2005). Profiles of air temperature were measured using unventilated, 100  $\mu$ m copper-constantan thermocouples mounted beneath radiation shields on the mast. High-precision water vapour and trace gas profiles including CO<sub>2</sub>, H<sub>2</sub>O, CH<sub>4</sub>, N<sub>2</sub>O, CO and the isotopologues HDO and <sup>13</sup>CO<sub>2</sub> were measured from 7 sampling heights (2.0, 4.4, 10.4, 26.3, 35.4, 43.4, 70.1 m) on the mast during a two-week campaign (13–26 November 2006), using two portable Fourier transform infrared (FTIR) spectrometers. The FTIR measurements are described in detail in the appendix. Separate instruments were used for H<sub>2</sub>O and trace gases so that the air could be dried for more accurate CO<sub>2</sub> analysis. Each height of the 7-point profile was sampled by both analysers for 2 min out of each 30-min period required to analyse the entire profile. The time series of concentrations at each level were interpolated linearly in time and re-sampled at the nearest integral hour to produce quasi-instantaneous vertical profiles. Hourly ensemble mean profiles for comparison with model output were constructed by selecting times when the gradient Richardson number  $Ri \leq 1.0$  at any height below 70 m, referencing the corresponding vertical concentration profiles to the value at the 40 m height (canopy top) and averaging them. The Richardson number,  $Ri = (g/\theta)(\partial\theta/\partial z)/(\partial\bar{u}/\partial z)^2$  was evaluated from mean hourly, 8-point vertical profiles of horizontal wind-speed and potential temperature,  $\theta$  measured at 0.55, 4.8, 10.6, 26.0, 34.7, 42.4, 55.7 and 70.0 m. Partial derivatives were estimated by differentiating cubic spline interpolants of the profiles. The above selection criterion ensured that our analysis was restricted to periods of fully coupled flow within and above the canopy and hence that LNF theory was applicable.

Three-dimensional sonic anemometers (CSAT-3, Campbell Scientific, Logan, UT; and HS-50, Gill Instruments Ltd., Lymington, UK) were used to measure  $w$  at 8 heights (0.5, 1.9, 11.1, 18.7, 27.2, 35.0, 43.5, 70.0 m) within and above the canopy. The data from the sonic anemometers were used to calculate profiles of  $T_E$  using Eq. (8) and thence a prior estimate of  $T_L$  (Eq. (7)). CO<sub>2</sub> fluxes at the ground were measured using an infra-red gas analyser attached to ten automated, pneumatic open-and-close chambers (Fest et al., 2009) and found to agree well with CO<sub>2</sub> fluxes from the ground derived from air temperature and soil moisture data via a correlation developed from earlier static chamber measurements using absorption of CO<sub>2</sub> by soda lime (Keith and Wong, 2006).

### 3.2. Other measurements of $\delta D$ in H<sub>2</sub>O

#### 3.2.1. Soil chamber

The soil chamber was used to obtain measurements of  $\delta D$  of soil evaporate in a controlled environment for the purpose of testing in isolation the soil component of the isotopically enabled SVAT model. The soil chamber consisted of a 1 m length of PVC pipe (diameter 15 cm), with one end inserted 2 cm into the soil, and an end-cap on the top. A fan was installed on the inside of the end-cap, and inlet and outlet tubes were inserted through holes in the end-cap and extended half-way down the chamber. The inlet

tube was supplied with air from a sampling point at 26.5 m on the tower, while the outlet tube was connected to a rotary pump, which flushed the chamber at a rate of 3 L min<sup>-1</sup>. At two-hourly intervals, and within 10 min of the 26.5 m tower line being sampled, air from the outlet tube was sampled by the FTIR. This allowed the  $\delta D$  of the soil evaporate in the chamber to be computed as (Evans et al., 1986):

$$\delta D_{\text{evap}} = \frac{\delta D_{\text{out}} \chi_{\text{H}_2\text{O},\text{out}} - \delta D_{\text{in}} \chi_{\text{H}_2\text{O},\text{in}}}{\chi_{\text{H}_2\text{O},\text{out}} - \chi_{\text{H}_2\text{O},\text{in}}} \quad (11)$$

Here,  $\chi_{\text{H}_2\text{O}}$  is the mole fraction of water vapour in dry air; “in” refers to air entering the chamber and “out” refers to the well-mixed air leaving the chamber.

### 3.2.2. Branch enclosures

Branch enclosures were installed to allow measurement of  $\delta D$  in transpirate ( $\delta D_{\text{trans}}$ ). The purpose of this was to produce a time series of daily flux-weighted values of  $\delta D_{\text{trans}}$  as estimates of  $\delta D$  in xylem ( $\delta D_{\text{xylem}}$ ), for use as input to the leaf component of the isotopically enabled SVAT model. Each branch enclosure consisted of a shaded 12.5 L transparent polyethylene cylinder with a fan, an inlet tube and an outlet tube. Pairs of branch enclosures, one empty reference enclosure and one enclosure containing a small branch, were installed at 1.5 m height in a young sapling and at 20 m height in a mature tree. Each enclosure was flushed continuously at 3 L min<sup>-1</sup> with ambient air. At two-hourly intervals, air from the outlet tubes of the reference and sample enclosures was sampled sequentially by the FTIR. This allowed the  $\delta D$  of the transpirate in the branch enclosure to be computed using Eq. (11), with “in” referring to air from the reference enclosure and “out” referring to air from the sample enclosure. The reference enclosure was used to insure that the “in” and “out” air streams were subjected to the same buffering volume.

### 3.2.3. Leaf and xylem water

Deuterium contents of leaf and xylem water were measured for the purpose of testing in isolation the leaf component of the isotopically enabled SVAT model. Measured  $\delta D_{\text{xylem}}$  was also used to initialise the  $\delta D$  profile of the modelled soil water. Triplicate leaf samples were collected from saplings at three-hourly intervals during the leaf-level gas-exchange measurement period (midday 16 November (doy 320)–midday 18 November (doy 322) 2006). Traces of the leaves' outlines were recorded to determine leaf area. The leaves were then picked, folded and stored frozen in gas-tight collection vials. Simultaneously, triplicate samples of sapling xylem were similarly stored. Less frequent samples of xylem from a mature tree (the same tree as that on which the branch enclosures were installed) were also obtained. Tissue water was extracted from leaves and xylem by vacuum distillation. Leaf water volume was determined and  $\delta D$  of the water samples was measured using a continuous-flow isotope ratio mass spectrometer (Isoprime, Micro-mass, Middlewich, UK). Xylem water fraction of bulk leaf water was determined from separate leaf samples.

### 3.2.4. Leaf-level gas-exchange

Before leaves were picked for isotopic analysis, exchanges of water vapour and CO<sub>2</sub> were measured for each leaf sampled using a LiCor 6400 (LiCor, Lincoln, NE). The purpose of this was to obtain day and night time series of stomatal conductance and leaf temperature for use in validating the leaf-level model for the isotopic composition of leaf water (and hence transpirate) against observations.

## 4. Modelled source/sink distributions

In this section we briefly review the SVAT model, which was also used in Hav09, before describing extensions to enable prediction of  $\delta D$  in soil evaporate and transpirate ( $\delta D_{\text{evap}}$  and  $\delta D_{\text{trans}}$ ). We then present SVAT model predictions of the ground/canopy partition for CO<sub>2</sub>, sensible heat and latent heat, and the deuterium content of the transpirate and soil evaporate for the two-week campaign period.

### 4.1. SVAT model

Vertical source/sink distributions of heat, water vapour and CO<sub>2</sub> were predicted using a multi-layered canopy model originally developed by Leuning et al. (1995), with improvements described by Wang and Leuning (1998) and Haverd et al. (2007). The core of the model is a leaf-level sub-model that couples stomatal conductance, photosynthesis and energy partitioning in response to radiation absorption, temperature and water vapour pressure deficit at leaf surfaces. Four key parameters in the sub-model were estimated by minimizing a cost function of residuals between predicted and net fluxes (of  $H$ ,  $\lambda E$  and  $F_c$ ) measured above the canopy.

The radiation sub-model, based on the two-stream approximations of Goudriaan and van Laar (1994), was used to calculate the rates of radiation absorption by sunlit and shaded leaves and by the soil in the visible, near-infrared and thermal wavebands. The leaf angle distribution parameter in the submodel for radiation transfer within the canopy (Sellers, 1985) was optimised independently, to minimize the residuals between model estimates and measurements of  $P_{\text{gap}}$  (Jupp et al., 2009), the probability of a direct beam not intercepting vegetation, at a range of view angles and heights. The mean vertical leaf area density profile, that was obtained by Jupp et al. (2009) from  $P_{\text{gap}}$  using in-canopy Lidar measurements, was a direct input to the model, as were local hourly meteorological data, and local hourly measured vertical profiles of air temperature, water vapour and CO<sub>2</sub> concentrations.

Respiration rates of soil and vegetation were calculated using functional relationships between respiration and soil and air temperatures obtained from chamber measurements (Keith and Wong, 2006).

Fluxes of sensible and latent heat at the soil surface were calculated using a soil model called Soil-Litter-Iso (Haverd and Cuntz, 2010). This is an extension of the one-dimensional model for coupled transport of heat and water in soil and litter (used in Hav09) to include coupled transport of stable isotopes (HDO and H<sub>2</sub><sup>18</sup>O).

### 4.2. Isotopically enabled soil model

Soil-Litter-Iso is a one-dimensional model for coupled transport of heat, water and stable isotopes (HDO and H<sub>2</sub><sup>18</sup>O) in soil and litter. Given inputs of net radiation absorption, water uptake by roots and below-canopy meteorological forcing (precipitation, wind speed, air temperature), it produces estimates of vertically resolved fluxes and stores of heat, soil moisture and the minor stable isotopologues of water. The model includes the complexity of coupled heat and water transport, enabling decomposition of the total moisture flux into liquid and vapour components. Resolution of the vapour phase is particularly important for predicting steep near-surface gradients in the concentration profiles of the minor isotopic species, which in turn strongly influence the isotopic content of the evaporative flux. The numerical implementation is based on Ross' fast solution to the Richards equation (Ross, 2003). It also incorporates explicit solution of the energy and moisture conservation equations at the soil/air interface, enabling resolution of temperature, humidity and isotopologue concentration at the interface (as distinct from the bulk quantities in the top soil layer).

#### 4.3. Isotopically enabled leaf model

Estimates of the deuterium content of the transpirate were obtained using an advection–diffusion model for transport of water isotopes in leaves (Cuntz et al., 2007). This calculates the isotopic gradient between leaf incoming xylem water and water at the evaporating site using leaf characteristics and boundary conditions, i.e. the meteorologic and isotopic environment. Leaf characteristics are, for example, the asymmetry between abaxial and adaxial mesophyll cell volume, which were derived from the literature (James and Bell, 2001). Environment variables include atmospheric relative humidity but also the isotopic composition of water vapour, for example. In contrast to Cuntz et al. (2007), we used kinetic fractionation factors of Merlivat (1978) that were confirmed by Luz et al. (2009).

The leaf characteristic length for water diffusion  $L_{\text{eff}}$ , was fitted against bulk leaf water observations of  $\delta\text{D}$  (Section 4.4.2). This effective length was then used for calculation of  $\delta\text{D}$  of the transpirate at each canopy level. The model also requires the  $\delta\text{D}$  of xylem water, which was estimated from a combination of measurements of transpirate in branch enclosures and xylem samples (see Section 4.5). Atmospheric conditions ( $\text{H}_2\text{O}$  and  $\text{HDO}$  concentrations, air temperature) were measured and stomatal conductance and leaf temperature calculated by the SVAT model.

#### 4.4. Validation of soil and leaf isotopic components of SVAT model

Here we validate the predictions of  $\delta\text{D}_{\text{evap}}$  and  $\delta\text{D}_{\text{trans}}$  from the soil and leaf models using measurements of  $\delta\text{D}$  in soil chamber evaporate and leaf water respectively. The soil model requires as input an initial vertical profile of  $\delta\text{D}$  of soil water. For this we assume a uniform value corresponding to that of the xylem water ( $\delta\text{D}_{\text{xylem}}$ ) at the start of the simulation period (doy 322). The leaf model also uses the measured value of  $\delta\text{D}_{\text{xylem}}$ , both as an initial estimate of the deuterium content of the leaf water, and as the value for xylem water in the model (which was assumed constant over the two-day validation period). Error-weighted combination of measurements of  $\delta\text{D}$  in xylem water from sapling and mature tree samples on doy 322 led to a value of  $-46.5 \pm 5\%$ .

##### 4.4.1. Validation of predictions of $\delta\text{D}$ in soil evaporate

Fig. 1(i) shows  $\delta\text{D}_{\text{evap}}$  inside the soil chamber over a ten-day measurement period. Air temperature was not measured, but estimated via a chamber surface energy balance, knowing the radiation flux at the chamber surface and the air flow rate through the chamber, and assuming no change in heat storage and an albedo of 0.7. Another unknown was the resistance between the soil surface and the bulk flow in the chamber, largely influenced by the fan on the roof of the chamber. We adjusted this parameter to a value of  $3 \text{ m}^{-1} \text{ s}$ , which optimised agreement between modelled and observed latent heat fluxes. In spite of these approximations, the major features of the measured time series of  $\delta\text{D}_{\text{evap}}$  are well captured by the model. In particular the magnitude of the rise in  $\delta\text{D}_{\text{evap}}$  over the first three days, corresponding to the first phase of drying, is well simulated. Also, the magnitudes of the diurnal variations, resulting from fluctuating relative humidity, are well reproduced by the model. Finally, the absolute values of the observations and predictions are in good agreement, justifying our choice of initial  $\delta\text{D}$  profile in the soil water.

##### 4.4.2. Validation of predictions of $\delta\text{D}$ in leaf water (and hence transpirate)

We used the measurements of  $\delta\text{D}$  in xylem water for doy 322 of  $-46.5 \pm 5\%$  together with leaf-level gas exchange (Section 3.2.4) and the FTIR spectrometer measurements of atmospheric  $\delta\text{D}$  to model the isotopic composition of mesophyll water. Further

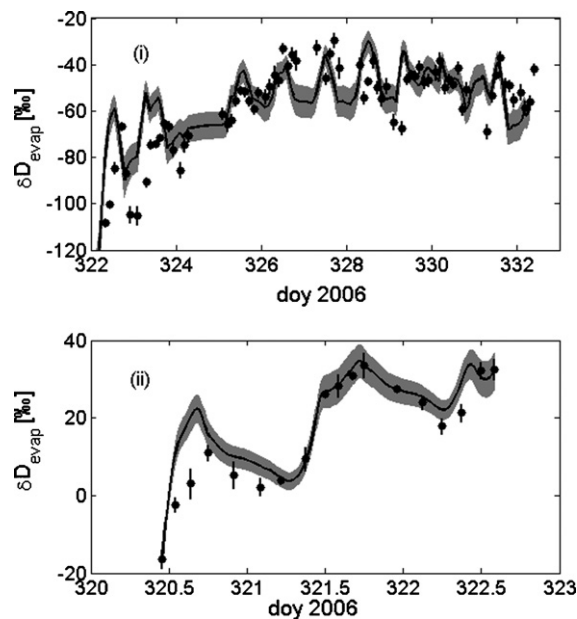


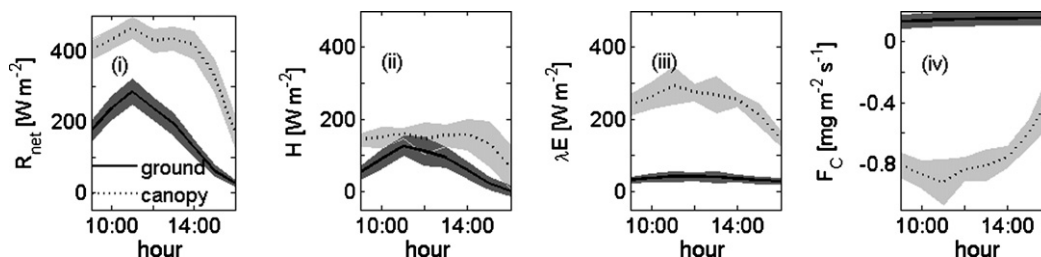
Fig. 1. Deuterium content of: (i) soil evaporate inside soil chamber; (ii) leaf water in sapling leaves. Symbols are observations with error bars representing one standard error. The shading for  $\delta\text{D}_{\text{evap}}$  represents the standard error propagated from errors in the initial estimate of  $\delta\text{D}$  in the soil water profile. For  $\delta\text{D}_{\text{leaf}}$ , the model standard error is propagated from the standard error in  $\delta\text{D}_{\text{xylem}}$ .

model inputs were the volumetric leaf water content determined as  $10.7 \pm 0.4 \text{ mol m}^{-2}$  and the amount of mesophyll on bulk leaf water, estimated to be around 10% from literature leaf characteristics (James and Bell, 2001). The effective length of water diffusion in leaves was fitted by comparing modelled and measured bulk leaf water isotopes to  $L_{\text{eff}} = 17 \text{ mm}$ . Fig. 1(ii) shows the time evolution of modelled against measured leaf water isotopes  $\delta\text{D}_{\text{leaf}}$ . The model captures the major features of the measurement time series. The good agreement at the end of nights reflects good accuracy in the measurements of  $\delta\text{D}$  in atmospheric water vapour (by FTIR) since night-time values mainly dependent on this variable. The day-time values, which depend on  $\delta\text{D}_{\text{xylem}}$ , atmospheric  $\delta\text{D}$ , humidity,  $L_{\text{eff}}$ , and gas exchange parameters, are well reproduced, except at the beginning of the simulation. Also, the overnight decrease in  $\delta\text{D}_{\text{leaf}}$ , which is highly dependent on night-time stomatal conductance, is well represented by the model, giving confidence in our leaf-level gas exchange measurements, especially at night, when small conductances can be difficult to measure.

#### 4.5. SVAT model predictions of source/sink distributions

Fig. 2 shows the ground/canopy partitions for  $R_{\text{net}}$ ,  $H$ ,  $\lambda E$  and  $\text{CO}_2$ . These are very similar to those presented in Hav09, with slight differences arising from modifications to the soil module. Note that the sensible and latent heat partitions are prior estimates, to be adjusted using the  $\chi_{\lambda E}$  parameter during the optimisation of modelled vertical concentration profiles against observed ones.

We now turn to the SVAT model predictions of  $\delta\text{D}_{\text{evap}}$  and  $\delta\text{D}_{\text{trans}}$ . Fig. 3(i) (dotted line) shows the time course of  $\delta\text{D}_{\text{xylem}}$  used as input to the leaf level model, as well as the corrected daily branch enclosure estimates from which it is derived. Specifically, the leaf water input from the xylem was determined as the flux-weighted mean of transpired water in the branch enclosures, corrected by an offset ( $-6\%$ ) to direct xylem isotope measurements. Fig. 3(ii) shows the modelled time series of  $\delta\text{D}_{\text{evap}}$  and  $\delta\text{D}_{\text{trans}}$ .  $\delta\text{D}_{\text{trans}}$  was modelled for each of 20 heights in the canopy, using leaf temperature and stomatal conductance at each height from the SVAT model, and



**Fig. 2.** Modelled ground/canopy sources, averaged over 11 clear-sky days during the period doy 322–332, 2006. (i) Net radiation absorption; (ii) sensible heat flux; (iii) latent heat flux; and (iv) CO<sub>2</sub> flux. Shaded areas represent standard errors on the mean, with contributions from uncertainties in the leaf area density distribution profile and net fluxes above the canopy the ground CO<sub>2</sub> flux.

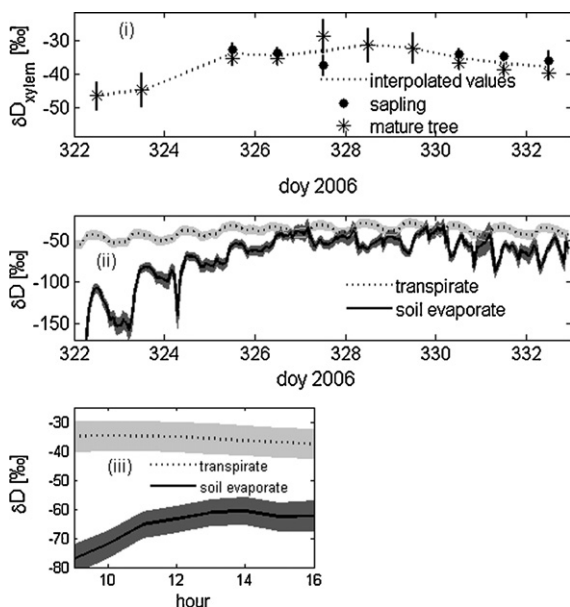
observed vertical atmospheric profiles of  $\delta D$  and humidity interpolated to the same 20 heights.  $\delta D_{trans}$  typically increased by about 1.1‰ for sunlit and 3.5‰ for shaded leaves from the bottom to the top of the canopy around noon, and the values presented here are the flux-weighted mean values for the whole canopy.  $\delta D_{trans}$  exhibits an increase over the first four days of the simulation, corresponding to the increase in  $\delta D_{xylem}$  over the same period. The diurnal variations result from non-steady state effects and hence in day-time values of  $\delta D_{trans}$  that are slightly higher and night-time values that are slightly lower than  $\delta D_{xylem}$ .  $\delta D_{evap}$  shows a much steeper rise in the first four days, and this is because, during the first phase of drying, the surface soil moisture available for evaporation becomes enriched much more rapidly than the xylem water. While the isotopic model output are presented as  $\delta D$ , we used model predictions of the HDO source distribution for modelling the atmospheric HDO concentration profile via Eq. (2), with subsequent conversion to  $\delta D$  for optimisation against observations.

Isotopic disequilibrium between the evaporation and transpiration components is a necessary condition for deuterium content of water vapour to provide additional constraint on the partition of *ET*. At doy 327, the night-time values of  $\delta D_{evap}$  and  $\delta D_{trans}$  approach each other, but there is still a strong disequilibrium between the daytime values. The strong day-time disequilibrium is further illustrated by Fig. 3(iii). Here hourly ensemble values of  $\delta D_{evap}$  and  $\delta D_{trans}$  have been constructed by detrending

(subtracting the daily mean from) the hourly values, taking ensemble averages over each hour of day and then adding the mean value for the whole time series. Again, the results indicate a significant disequilibrium between  $\delta D_{evap}$  and  $\delta D_{trans}$ . We also see here a strong increase of  $\delta D_{evap}$  during the day and a slight decrease in  $\delta D_{trans}$ . Flux-weighted mean values of  $\delta D_{evap}$  and  $\delta D_{trans}$  for the period doy 322–332 reveal a 24‰ disequilibrium between the components of the mean water vapour flux.

Historically, most isotope-based separations of transpiration and evaporation (Ferretti et al., 2003; Moreira et al., 1997; Williams et al., 2004; Xu et al., 2008; Yakir and Wang, 1996; Yopez et al., 2005) have relied on much simpler estimates of the isotopic content of the soil evaporate. These involve applying the Craig and Gordon equation (Craig and Gordon, 1965) (which accounts for equilibrium and diffusive fractionation effects), assuming the isotopic content of the liquid water is that of the soil moisture in the top few cm of soil, or at the evaporating front, or integrated over the soil column. We estimated  $\delta D_{evap}$  by this method, using  $\delta D$  of liquid water from the modelled soil moisture profiles. The results deviated from those in Fig. 3(ii) by at least 70‰. This highlights a large source of uncertainty associated with estimating the isotopic content of the soil evaporate using the isotopic composition of water extracted from soil samples.

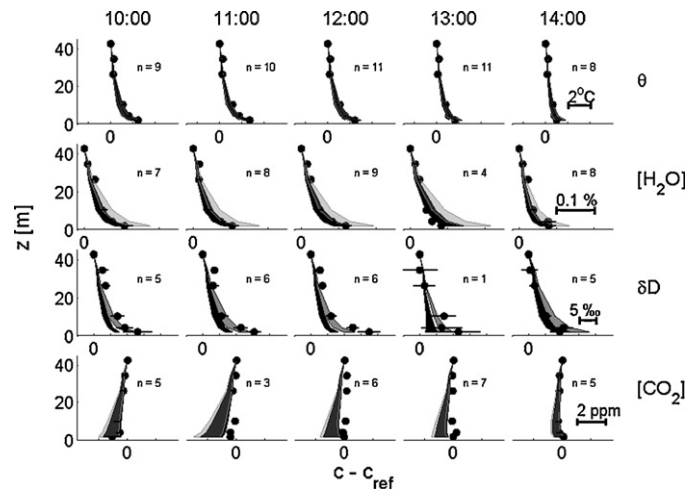
**5. Results and discussion**



**Fig. 3.**  $\delta D$  content of (i) xylem; (ii) modelled soil evaporate; and (iii) modelled transpire. Xylem values are interpolated from flux-weighted measurements of  $\delta D$  in transpire from two branch enclosures. Shading represents standard errors, as in Fig. 1.

Fig. 4 shows the hourly ensemble mean modelled and measured vertical profiles of potential temperature, water vapour,  $\delta D$  in water vapour and CO<sub>2</sub>, referenced to their values at the top of the canopy (40 m). Model profiles were generated using optimised parameters  $c_1$ ,  $c_2$  (Eq. (6)) and  $x_{\lambda E}$ . Black and light shaded grey areas correspond to model predictions generated using parameters optimised with cost functions constructed with  $v = \{\theta, H_2O, CO_2\}$  and  $v = \{\theta, H_2O, CO_2, \delta D\}$  respectively. Overlap between the two sets of model predictions is represented by dark grey shading.

As in Hav09, the non-isotopic species are well simulated with  $v = \{\theta, H_2O, CO_2\}$ . However, the parameters which optimise the agreement between modelled and measured non-isotopic profiles, produce modelled  $\delta D$  profiles which significantly underestimate the increase of  $\delta D$  near the ground. When  $\delta D$  also contributes to the cost function: i.e.  $v = \{\theta, H_2O, CO_2, \delta D\}$ , model/measurement overlap for  $\delta D$  is much improved, while the predictions for the non-isotopic profiles overlap with the simulations which do not utilise  $\delta D$  information. The fitted parameters corresponding to the model predictions in Fig. 4 are given in Table 1, and the corresponding vertical profiles of  $T_L$  are shown in Fig. 5. Upon inclusion of  $\delta D$  in the cost function, the  $T_L$  profile shifts to lower values which are closer to the prior estimate and also closer to earlier theoretical estimates (see Hav09 and references therein) of  $T_L$  at the top of the canopy. The value of the normalised  $T_L$  at the top of the canopy in Fig. 5(i) ( $0.51 \pm 0.1$ ) is lower than that reported in Hav09 ( $0.66 \pm 0.1$ ). This difference is largely attributable to different weighting coefficients



**Fig. 4.** Mean measured profiles (dots) and corresponding predicted vertical profiles of potential temperature, water vapour,  $\delta D$  of water vapour, and  $CO_2$  concentration. Predictions using parameters obtained with  $v = \{\theta, H_2O, CO_2\}$  are in black; predictions using parameters obtained with  $v = \{\theta, H_2O, CO_2, \delta D\}$  are in light grey. Overlapping predictions are in dark grey. The shaded areas represent standard error bounds on model profile predictions, with errors propagated from standard errors in the modelled vertical source distributions.

**Table 1**  
Optimised parameter values for coefficients in the  $T_L$  parameterisation and the parameter for adjusting the latent heat flux at the soil.

	Prior	Optimised (no $\delta D$ )	Optimised ( $\delta D$ included)
$c_1$	7.32	$6.6 \pm 3$	$7.1 \pm 2$
$c_2$	0.32	$0.51 \pm 0.1$	$0.41 \pm 0.1$
$x_{\lambda E}$	0.0	$0.09 \pm 0.06$	$-0.02 \pm 0.07$

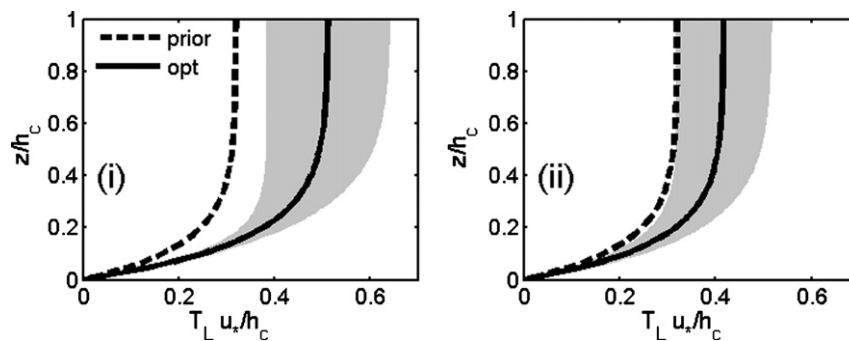
for the two studies: in this work we constructed the cost function such that each species contributes equally to the prior cost, whereas in Hav09, each profile point was weighted according to model and measurement uncertainty. The high sensitivity of estimated parameters to cost function formulation is discussed in detail by Trudinger et al. (2007).

Qualitatively,  $T_L$  is a measure of the persistence of the turbulence. Thus it is expected that lower values (corresponding to less efficient mixing) be required to match the steep gradients seen in the observed  $\delta D$  profiles. A corresponding over-prediction of the gradient in the water vapour profiles is avoided by adjusting  $x_{\lambda E}$  such that the latent heat flux at the ground is lower by 2% than the prior estimate. In contrast, in the case without  $\delta D$  in the cost function,  $x_{\lambda E}$  was adjusted such that the latent heat flux at the ground is higher than the prior value by 9%. The corresponding partitions of  $ET$  are given in Table 2, alongside the prior estimate. Uncertainty estimates are standard errors, propagated from uncertainties in source/sink distributions. Optimised values are revised estimates, obtained by multiplying the prior estimate by optimised  $(1 + x_{\lambda E})$ .

The values in Table 2 indicate that, in spite of very different  $\delta D$  profile predictions, the two optimised parameter sets yield partitions of  $ET$  which are indistinguishable within error bounds. The  $T_L$  profiles resulting from the two cases are also indistinguishable within uncertainty limits, although the case which utilises  $\delta D$  information yields slightly smaller uncertainty estimates. The reduction in uncertainty can be seen by comparing the shaded areas on the  $T_L$  profiles in Fig. 5(i) and (ii).

It is clear from the results presented above that both the partition of  $ET$  and the vertical profile of  $T_L$  are quite insensitive to the inclusion of  $\delta D$  in the parameter estimation process. Two possible reasons for this are suggested and investigated below.

The first possibility is that the other species already tightly constrain the parameters, such that there is little more to be gained by including the additional  $\delta D$  information. First, we investigated this by repeating the optimisation process with  $v = \{\delta D, H_2O\}$  in the cost function. This led to more uncertain parameter estimates: ( $c_1 = 31 \pm 30$ ;  $c_2 = 0.71 \pm 0.3$ ;  $x_{\lambda E} = -0.38 \pm 0.54$ ) compared to the case with  $v = \{\theta, H_2O, CO_2\}$  (see Table 1), indicating that the latter combination of observation types provides a relatively strong constraint. Second, we repeated the optimisation process with  $v = \{\theta, H_2O, CO_2, \delta D\}$ , this time with a 70% perturbation to  $\delta D_{evap}$ , consistent with errors associated with traditional approaches to estimating  $\delta D_{evap}$ , as discussed in Section 4.5. Surprisingly, even with this large perturbation to our estimate of  $\delta D_{evap}$ , we were still able to produce predicted profiles of all species which overlapped measurements within standard error bounds, and the parame-



**Fig. 5.** Prior and optimised estimates of  $T_L$ : (i) without including  $\delta D$  in cost function,  $v = \{\theta, H_2O, CO_2\}$ ; (ii) including  $\delta D$  in cost function,  $v = \{\theta, H_2O, CO_2, \delta D\}$ . Shaded areas represent standard errors, which arise from uncertainties in the vertical source/sink distributions and uncertainties in the retrieved parameters ( $c_1$  and  $c_2$  in Eq. (1)) for a given source/sink distribution.



**Table 2**  
Ground/canopy latent heat flux partition and ratio of transpiration to total latent heat flux: mean values for 11 clear-sky days during the period day 322–332, 2006.

	$\lambda E_{\text{prior}}$ ( $\text{MJ m}^{-2} \text{d}^{-1}$ )	$\lambda E_{\text{opt}}$ (no $\delta\text{D}$ ) ( $\text{MJ m}^{-2} \text{d}^{-1}$ )	$\lambda E_{\text{opt}}$ ( $\delta\text{D}$ ) ( $\text{MJ m}^{-2} \text{d}^{-1}$ )
Ground	$1.8 \pm 0.17$	$2.0 \pm 0.2$	$1.8 \pm 0.2$
Canopy	$10.3 \pm 0.5$	$10.1 \pm 0.5$	$10.3 \pm 0.5$
Transpiration fraction	$0.85 \pm 0.02$	$0.83 \pm 0.02$	$0.85 \pm 0.02$

ter estimates ( $c_1 = 7.1 \pm 4$ ;  $c_2 = 0.41 \pm 0.1$ ;  $x_{\lambda E} = -0.03 \pm 0.03$ ) were close to those obtained using our unperturbed estimate of  $\delta\text{D}_{\text{evap}}$ . This result indicates that a large change in the isoflux at the ground can be readily compensated for by small changes in  $x_{\lambda E}$  and the turbulence parameters, leaving the optimised modelled profiles little changed. These two investigations thus substantiate our first explanation, that our target parameters are well constrained by the non-isotopic observations.

The second possibility is that  $\delta\text{D}$  contributes only one quarter of the prior cost function. When we repeated the optimisation with  $v = \{\delta\text{D}, \text{H}_2\text{O}\}$  (with  $\delta\text{D}$  contributing to half of the prior cost function), we found that the estimated parameters were indeed sensitive to  $\delta\text{D}$  being given a higher weighting, but they were also less tightly constrained and the turbulence parameter values became extreme. Thus the second possibility is substantiated, but does not suggest that weighting  $\delta\text{D}$  more highly achieves better results.

## 6. Conclusion

The modelled vertical concentration profiles resulting from inclusion of  $\delta\text{D}$  in the cost function demonstrate our ability to make consistent estimates of both the scalar source distributions and the deuterium content of the water vapour sources. However, introducing measurements of deuterium in water vapour does not significantly alter resulting estimates of  $T_L$  and the partition of  $ET$ , compared with the case when only temperature, water vapour and  $\text{CO}_2$  concentration profiles are available. We propose a revised estimate of  $T_L$ , corresponding to that obtained using  $\delta\text{D}$  (see Table 1), since this result utilises all the experimental information available. The lack of significant difference between estimates of the partition of  $ET$  with and without  $\delta\text{D}$  (in spite of significant isotopic disequilibrium (ca. 24%) between  $ET$  components) arises because  $\delta\text{D}$  only contributes to one quarter of the prior cost function and because the  $ET$  partition is already well constrained by the fluxes of sensible heat,  $\text{CO}_2$  and water vapour, together with their associated measured concentration profiles and modelled source/sink distributions. The latter reason suggests that the additional data and modelling required to use deuterium are not warranted for the purpose of partitioning  $ET$  using the framework presented here.

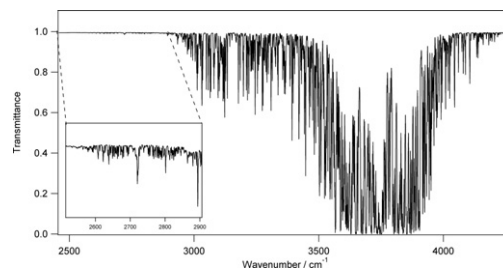
## Acknowledgements

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## Appendix A. Analysis of trace gases and isotopic ratios in air by FTIR spectrometry

### A.1. Introduction

Optical methods such as Fourier Transform Infrared (FTIR) or laser absorption spectrometry can be deployed in the field and used



**Fig. A1.** Infrared transmission spectra from 2500 to 4000  $\text{cm}^{-1}$  of  $\text{H}_2\text{O}$  (main trace) and HDO (inset trace) in natural abundance at typical atmospheric humidity.

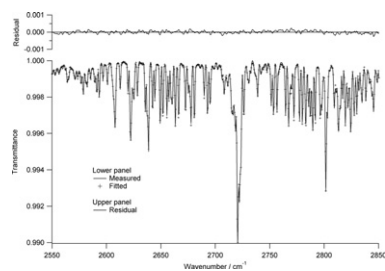
to analyse water vapour and other trace gases, including isotopologues, continuously in whole air samples. They can provide real time measurements and a much higher data density than conventional IRMS analysis, although in some cases with somewhat lower accuracy or precision per measurement.

FTIR spectroscopy measures the broad-band infrared absorption spectrum of an air sample, which can be analysed to retrieve concentrations of many compounds simultaneously. For an introduction to FTIR applications in atmospheric trace gas analysis, see reviews by Griffith (2002) and Griffith and Jamie (2000) and references therein. A more complete description and recent application to high accuracy clean air measurements is described by Griffith et al. (2010). In the case of D/H ratios in water vapour, FTIR spectroscopy measures the absolute concentrations of HDO ( $^2\text{H}^1\text{H}^{16}\text{O}$ ) and  $\text{H}_2\text{O}$  ( $^1\text{H}^1\text{H}^{16}\text{O}$ ) molecules directly in a whole air sample, from which the isotope ratio and  $\delta\text{D}$  is determined. Similarly,  $\delta^{13}\text{C}$  in  $\text{CO}_2$  is determined from measurements of the individual  $^{13}\text{CO}_2$  and  $^{12}\text{CO}_2$  isotopologues. The FTIR spectrometer is portable for field use, and no sample treatment is required – whole air is drawn through a sample cell and its IR spectrum is measured continuously in real time to provide the required analysis.

Due to the factor of two mass difference between D and H, the O–D stretching vibration of HDO is shifted by several hundred wavenumbers from that of O–H in  $\text{H}_2\text{O}$ , so that it (fortuitously) appears in an otherwise uncluttered region of the infrared spectrum. Fig. A1 illustrates the spectra and the regions used for  $\text{H}_2\text{O}$  and HDO analysis. The large separation between  $\text{H}_2\text{O}$  and HDO bands and lack of major interference from other molecules allows the use of a compact, low resolution spectrometer suited to field studies.

### A.2. FTIR instrumentation and measurements

Air was drawn continuously at  $2 \text{ L min}^{-1}$  from each of seven inlets on the tower at 2.0, 4.4, 10.4, 26.3, 35.4, 43.4, 70.1 m with a small membrane pump through identical lengths of 9.25 mm OD Dekabon™ tubing. All lines were heated up to the 40 m level to avoid condensation of water vapour in cold conditions near the ground. In each 30 min measurement cycle, air from each of the seven inlet lines was analysed sequentially to provide one seven-point vertical profile, allowing 250 s for each inlet line measurement. Within each 250 s sample period, the spectrometer cell was rapidly evacuated (4-stage membrane pump, Brand MV2) and re-filled from the next inlet line to be analysed. A steady flow of  $2 \text{ L min}^{-1}$  from the inlet line and cell was then established and the FTIR spectrum recorded for the last 120 s of the 250 s period. The



**Fig. A2.** Example of a spectral fit in the HDO fitting region. In the lower plot the solid line is the measured spectrum and the crosses are the fitted spectrum. The upper trace is the difference between measured and fitted spectra.

analysis of each spectrum to provide component concentrations and  $\delta D$  values was performed in real time (as described below) at the end of each 250 s sample period. All valve switching, pressure and temperature measurements, spectrometer operation and spectrum analysis were carried out automatically under control of a single Visual Basic program running on a laptop PC. Results were displayed in real time and could be downloaded at any time for further analysis on a separate PC.

Two FTIR analysers were employed; in one the airstream was flowed undried through the sample cell for water vapour and  $\delta D$  analysis, in the other the air stream was dried by a Nafion® membrane drier (Permapure PD-100T24MSS, NJ, USA) and magnesium perchlorate trap for more accurate analysis of other trace gases.

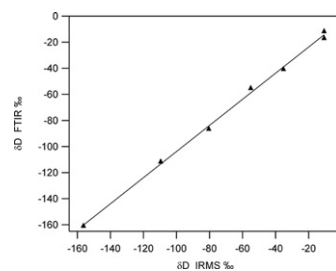
The FTIR spectra were recorded from 2000 to 5000  $\text{cm}^{-1}$  at 1  $\text{cm}^{-1}$  resolution with Bruker IRCube FTIR spectrometers (Bruker Optics, Ettlingen, Germany) fitted with TE-cooled, mercury cadmium telluride (MCT) detectors (J19TE3, 5  $\mu\text{m}$  cutoff, Judson Technologies, PA, USA) to obtain a high signal:noise ratio, and with 26 m multipass White cells (model PA26, volume 3.5 L, Infrared Analysis Inc. CA, USA) to enhance the IR absorption of HDO (Fig. A1). The spectrometer and cell were thermostatted to 34 °C to ensure stability and avoid temperature-dependent calibration fluctuations. The IR beam path through the spectrometer and outside the sample cell was purged with nitrogen to remove interference from  $\text{CO}_2$  and water vapour outside the sample cell. The spectrometers and sampling system operated continuously and automatically for the entire period of the campaign.

### A.3. Spectrum analysis

Spectra were analysed by a non-linear least squares fitting technique, in which the measured FTIR spectrum is fitted with an iteratively calculated spectrum until a least-squares best fit is obtained. The concentrations of absorbing molecular species were determined from the values which achieve best fit to the measured spectrum. For further details see (Feilberg et al., 2002; Griffith, 1996). In the spectral region 2000–5000  $\text{cm}^{-1}$  collected by the spectrometer, HDO was fitted in the region 2600–2840  $\text{cm}^{-1}$ ,  $\text{H}_2\text{O}$  and  $\text{CH}_4$  from 2940 to 3156  $\text{cm}^{-1}$  (see Fig. A1), and  $\text{CO}_2$ ,  $\text{CO}$  and  $\text{N}_2\text{O}$  from 2102 to 2320  $\text{cm}^{-1}$ . An example of a fitted spectrum in the HDO region is shown in Fig. A2, which displays the measured, fitted and residual spectra. The calculation is sufficiently accurate to fit the measured spectrum to close to its noise level.

### A.4. Calibration

The least squares fitting procedure used for quantitative spectrum analysis is based on tabulated spectral data (HITRAN 2004; Rothman et al., 2005) and requires no calibration gases; it provides a working calibration for trace gas concentrations and  $\delta D$  which is usually accurate to better than 5% and precise to ca. 0.1% for  $\text{H}_2\text{O}$ , HDO,  $\text{CO}_2$ ,  $\text{CH}_4$  and  $\text{N}_2\text{O}$  at ambient levels (Esler et al., 2000;



**Fig. A3.** Calibration of FTIR measurement of  $\delta D$  on 10 November 2006. X axis:  $\delta D$  values of reference water samples determined by IRMS. Y axis: FTIR measurements. The regression equation is  $y = 1.001x - 3.26$  and standard error of prediction is 2.7%.

Griffith, 1996). For more accurate absolute calibration, measurements must be compared to independently calibrated reference gases. For  $\text{CO}_2$ ,  $\text{CH}_4$  and  $\text{N}_2\text{O}$ , measurements of two reference tanks of air calibrated in CSIRO's GASLAB were performed in the field before, during and after the campaign period. The calibration drifts were less than 1% over the 16-day duration of the campaign and a time-dependent calibration factor was applied to all data to bring them to the common calibration scale.

For water vapour mixing ratios, the difficulty of introducing air with accurately known water vapour concentrations into the measurement cell, and adsorption and memory effects of cell and tubing walls, precluded calibration under field conditions. We therefore rely on the spectral fitting alone for calibration with uncertainty estimated to be at most 5% as described above (see also Smith et al., 2010). In the previous work we demonstrated this level of accuracy in a similar measurement situation by comparison of FTIR measurements of water vapour on a 22 m tower with Vaisala Humitter sensors (Griffith et al., 2002). In the present work, we have compared the FTIR measurements of water vapour with those from an infrared gas analyser (LI6262, Licor Inc., Lincoln, Nebraska) which sampled air from the same heights on the tower. These comparisons are consistent with the quoted 5% accuracy for the FTIR measurements.

Calibration for  $\delta D$  in water vapour presents a more difficult challenge, since calibrated isotopic reference water samples are available as liquid water but the FTIR analysis is fundamentally a vapour measurement. To calibrate for  $\delta D$ , we measured the FTIR spectra of up to ten liquid water samples of known  $\delta D$  (V-SMOW) analysed by isotope ratio mass spectrometry at CSIRO Land and Water, Adelaide. The liquid samples were quantitatively vapourised into a continuous flow of 2–4  $\text{L min}^{-1}$  dry air from a high pressure tank in a heated block at 120 °C to provide mixing ratios typical of the air samples to be measured – 0.5–1.5 mol%. Each reference water sample flowed through the spectrometer cell until the real-time-indicated  $\delta D$  was steady, typically 25–30 min per sample. Raw FTIR measurements were corrected for a small dependence on the absolute water vapour concentration. A typical calibration of FTIR vs IRMS is shown in Fig. A3. Calibration was performed before, during and after the campaign. The standard error of prediction from the regressions is typically 1–3% for 2 min measurements of  $\delta D$ , and FTIR values of  $\delta D$  in this work have analytical precision of this order. Wall memory effects in the cell and tubing which differ between  $\text{H}_2\text{O}$  and HDO molecules may add further uncertainty in accuracy which we estimate to be of the same order.

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